

ULTRA-WIDEBAND COMMUNICATIONS
SYSTEM AND METHOD USING A DELAY
HOPPED, CONTINUOUS NOISE
TRANSMITTED REFERENCE

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH &
DEVELOPMENT

[0001] The U.S. Government may have certain rights in this invention pursuant to the National Institute of Standards and Technology Contract Number 70ANB0H3035 awarded by NIST.

BACKGROUND OF THE INVENTION

[0002] This invention relates to the transmission, reception, detection, synchronization, and use of ultra-wideband communication systems. In particular, it pertains to a continuous noise transmitted-reference, delayed hopped (TR/DH) ultra-wideband radio communications system.

[0003] Conventional ultra-wideband (UWB) radio systems operate by transmitting and receiving a sequence of very short radio frequency (RF) pulses, the duration of which is typically less than a nanosecond. This is referred to as impulse radio. The individual pulses typically have low energy. Consequently, the low duty cycle of the pulsed waveform results in a very low average power.

[0004] One conventional approach to implementing UWB communications systems is to utilize a pulse position modulation (PPM) scheme to impress information onto a UWB carrier. PPM is an orthogonal signaling scheme by which a receiver determines in which one of a number of different time windows a received pulse appears, and this determination conveys a quantum of information, e.g., if there are two possible time windows, determination of one window conveys one bit of information; for three windows, a trit of information is conveyed, for four windows, two bits, and so on.

[0005] Successful operation of a PPM system requires accurate time synchronization be acquired and maintained between transmitter and receiver. For example, for an UWB PPM system, this synchronization must be accurate to within a fraction of the pulse duration. Because the pulse duration is quite small in a UWB system, the synchronization requirements are quite stringent. The time required to establish synchronization for this method can be prohibitive, and acquisition is not always possible in the presence of multiple access interference, which occurs when more than one pair of transmitters and receivers is active at the same time. A long acquisition time is a major risk in the use of conventional UWB impulse radio communications. Therefore, a need exists for UWB communication systems without the synchronization difficulties associated with conventional approaches.

BRIEF SUMMARY OF THE INVENTION

[0006] The present invention consists of the combination of two chief features and innovations surrounding each of them. The first of these is known in the art as transmitted-reference (TR). The TR technique is defined as the transmission of two versions of a wideband carrier, one modulated by data and the other unmodulated. These two signals are recovered by the receiver and are correlated with one another to perform detection of the modulating data. The commonly used wideband carrier is a continuous, wideband pseudo-noise source, and the modulated and unmodulated versions are typically separated from one another in either time or frequency. In the present invention, the carriers used are continuous, wideband noise or continuous, wideband pseudo-noise. Thus, in the present invention, the term "transmitted-reference" refers to the transmission and reception of multiple instances of a noise or pseudo-noise waveform that are separated from each other by specific time intervals, known to the receiver. The noise waveform by itself is referred to as the carrier. Information is carried by such a signal by modulating the relative phase of the two transmitted noise waveforms. The receiver correlates the received signal with a delayed version of itself over a finite interval to demodulate the signal. In contrast to impulse radio methods, the use of the transmitted-reference technique makes synchronization with the individual pulses unnecessary. On the other hand, it also

imposes a signal-to-noise ratio (SNR) penalty when compared with impulse radio techniques.

[0007] When two UWB TR signals are generated with different delays, it is possible, under certain conditions, to receive and demodulate both of them simultaneously, by applying two separate correlators to the same received signal. Thus, the use of different delays, each associated with a separate transmitter, imparts a certain amount of multiple access capacity to an UWB TR communications system. In one embodiment, "capacity" is defined as the supportable number of simultaneous users of the communications system.

[0008] The second feature of the present invention is a type of multiple access scheme called "delay hopping". In the context of UWB communications, delay-hopping refers to the method of varying the delay used in the TR UWB transmission in a fixed pattern known both to the transmitter and to the receiver. This pattern constitutes a code word, and multiple access capacity is obtained through the code-division multiple access (CDMA) technique.

[0009] CDMA is a multiple access method that allows users to access the channel in a random manner. Signal transmissions from different users can completely overlap in both time and frequency in a CDMA system. The demodulation of these signals makes use of the fact that each signal is associated with a code sequence known to the receiver, and this code is usually referred to as a spreading code. Spreading codes of different transmitters should be orthogonal (or nearly so) in the sense that multiple codes can be detected simultaneously with little interference to one another.

[0010] One representative embodiment of the present invention consists of combining the TR and DH techniques to create a UWB communications scheme for transmitting a continuous noise transmitted reference that is easy to synchronize and has a usable level of multiple access capacity.

BRIEF DESCRIPTION OF THE DRAWINGS

[0011] Figure 1 is a block diagram of one representative embodiment of a transmitter for transmitting a continuous noise, delay hopped, transmitted reference.

[0012] Figure 2 is a block diagram of another representative embodiment of a transmitter for transmitting a continuous noise, delay hopped, transmitted reference.

[0013] Figures 3 is a block diagram of one representative embodiment of a receiver.

[0014] Figures 4 is a block diagram of one representative embodiment of a bank of correlators.

[0015] Figure 5 is a block diagram of one representative embodiment of a CDMA code word correlator.

[0016] Figure 6 is a block diagram of another representative embodiment of a receiver.

[0017] Figure 7 is a diagram of the power spectral density of a noise carrier.

[0018] Figures 8 is a diagram of the power spectral density of transmitted reference delay hopped modulated noise carrier.

[0019] Figures 9 is a diagram of a modulated signal.

[0020] Figures 10 is a diagram of the outputs of the correlator multipliers of one representative embodiment of the receiver.

[0021] Figures 11 is a diagram of the output of the integrator of one representative embodiment of the receiver.

[0022] Figure 12 is a diagram of an output of the CDMA code word correlator.

DETAILED DESCRIPTION OF THE INVENTION

[0023] In one embodiment, the specific transmitted-reference (TR) method described here requires the transmission of at least two continuous noise waveforms. The two continuous noise waveforms are separated by a time interval, D , known to both the receiver 300 (Fig. 3) and transmitter 100 (Fig. 1). The transmitted data is encoded by the relative amplitude polarity of the two continuous noise waveforms. One of the transmitted waveforms is always transmitted with the same polarity; this waveform is the reference signal and the other waveform, whose polarity is modulated, is the information-bearing signal. The name “transmitted-reference” comes from the fact that the reference signal is transmitted along with the information-bearing signal.

[0024] As shown in Fig. 1, one embodiment of a transmitter 100 used to transmit the continuous noise transmitted reference comprises a wideband noise source 110 connected to a delay 160 of delay time interval (D) and a summer 170. The output of the delay 160 is connected to information modulator 130 that is also connected to the summer 170. An antenna 180 is connected to the summer 170. In this embodiment, two instances of the continuous noise waveform are separated by delay time interval (D). The delay time interval (D) is known by the transmitter 100 and the receiver 300 (Fig. 3). The transmitted data is encoded by the relative amplitude polarity of the continuous noise waveforms.

[0025] In another embodiment of the transmitter 100, as shown in Fig. 2, a wideband noise source 110 is connected to a spectral shaping device 120 to produce a continuous noise carrier. The wideband noise source can comprise a back biased diode and passing the output of the diode through a capacitor to remove any DC bias. Also, the wideband noise source can comprise a high speed pseudo random noise generator. The spectral shaping device 120 filters the output of the wideband noise source 110. In one embodiment, the spectral shaping device 120 can comprise an analog filter. In another embodiment, the spectral shaping device 120 can comprise a digital filter. The spectral shaping device 120 removes energy from predetermined frequency bands to protect the integrity of the communication and/or to comply with

federal government regulations. The spectrally shaped continuous noise transmitted reference is provided to the summer 170 and information modulator 130.

[0026] In one embodiment, the information modulator 130 impresses a delay hop code division multiple access (CDMA) code word on the continuous noise carrier from the spectral shaping device 120. A delay hop controller 140 also connected to the multiplexer and data polarity switch 150 derives delay hop CDMA code word 135. Information symbols 145 are provided to the delay hop controller 140 that uses the information symbols 145 to generate the delay hop CDMA code word 135. This code word consists of a sequence of delay values and an associated sequence of chip polarities of phases. The delay hop controller 140, in one embodiment, comprises a finite state sequential machine. In one embodiment, the code word comprises N_C chips. Each of the N_C chips comprises a pair of continuous noise waveforms separated by a fixed time interval or delay.

[0027] The multiplexer and data polarity switch 150 controls the application and routing of the wideband continuous noise waveforms to a band of fixed delays 160 and the application of the chip polarity values to the information-bearing waveform. In one embodiment, the delays 160 can comprise discrete delay analog components, such as, sections of coaxial transmission cable. In another embodiment, the delays 160 can comprise digital delay components. In another embodiment, where the noise source 110 comprises a pseudo random noise source, the delays 160 can be created by the pseudo random noise source when the noise is generated. The multiplexer switch 150 is controlled by the delay hop controller 140 by generating the delay hop CDMA code words 135 according to predetermined design criteria as imposed by bounds on the cross-correlations of the delay hop CDMA code words 135. The output of the spectral shaping device 120 and the outputs of the fixed delays 160 are combined by a summer 170 and summed to produce a continuous noise transmitted reference signal that comprises a sum of two instances of the continuous noise carrier generated by the wideband noise source 110 wherein a first instance comprises an undelayed continuous noise waveform and the second instance comprises the delayed instance of the at least one of the continuous noise waveforms

impressed with the modulated delay hop CDMA code word 135. The continuous noise waveform is provided to filter 175 for further filtering and then is supplied to the antenna 180 and radiated.

[0028] Delay hopping is a code division multiple access (CDMA) scheme to be used with transmitted reference UWB. A limited amount of multiple access capacity is available in TR UWB by transmitting and receiving continuous noise transmitted reference signals with separate delays. A receiver 100 tuned to one delay will respond to received continuous noise transmitted reference signal at a separate delay at a far lower energy level than it would to continuous noise transmitted reference signals transmitted with its own delay value. However, when multiple transmissions with different delays are present at the receiver's antenna 310, spurious correlations between continuous noise transmitted reference signal originating from different transmitters can occur. By using CDMA code words whose chips represent a multiplicity of delays and a multiplicity of relative signal polarities between the reference and the information-bearing signal, delay hopping allows for a greater multiple access capacity than simply transmitting with different delays.

[0029] A transmitted reference/delay hopped (TR/DH) code word (also termed delay hop CDMA code word 135) consists of N_C chips, transmitted sequentially. Each of the N_C chips comprising a continuous noise transmitted reference separated by a fixed time interval. The continuous noise transmitted reference in different chip intervals are, in general, characterized by different delays. Note that the chip values are distinct both in associated delay value and in the polarity of the transmitted chip. When a code word of N_C chips is used to send one data bit, then if the data bit to be sent is a one, all information-bearing signals in each chip of the code word have the polarity of the code word polarity bit. If the data bit to be sent is zero, then all information-bearing signals in each chip of the code word are transmitted with the opposite polarity of the code word polarity bit.

[0030] Typical values of the parameters are as follows. The number of chips in a code word (N_C) will be in the range of 50 to 1000, and the duration of each chip will be in the range of 1 to 10 microseconds. The time delays separating the two



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delayed circuit path. This non-zero-mean product is integrated over a chip interval to produce a chip signal. Note that this circuit implements the mathematical operation of estimating the correlation of the received signal at a lag given by D .

[0034] The CDMA code correlator 340 will take samples of the multiple outputs of the bank of pulse pair correlators 320 and add them together in a manner dictated by the expected CDMA code word. The objective of this operation is to produce the registered sum of all the chip signals. When the expected code word matches the transmitted code word 135, this operation will have the effect of applying a gating waveform, matched to the entire delay hopped (DH) code word waveform, to the observed data at the output of the correlators 320. If the gating waveform matches the shape of the chip signal waveform, a matched filter is implemented; however, this requires knowledge of the relative timing of the sample clock and the transmitter chip clock. If the gating waveform applied to the individual chip is rectangular, with duration $2T_c$, then the effect of the CDMA code word correlator 340 is to add all of the individual chip waveforms in phase, producing an output which is a high-SNR version of the individual chip waveform.

[0035] In one embodiment, the structure of the CDMA code correlator is depicted in Figure 5. The specific code correlator 340 depicted uses a CDMA code word 135 that matches the correlator bank 320 output depicted in Figure 4. Note that the chip time delays ($D_{\text{chip time}}$) 342 and signs (additions and subtractions) cause the elementary correlator peaks to be aligned in time with the same signs. The delayed outputs of the A/D converters from the CDMA code word correlator are summed by summer 344 and provided as output 350. Since the sample period of the A/D converters 330 has been specified to be a fraction of the chip period, the delays 342 in Figure 5 may, in one embodiment, all be implemented as a number of digital storage devices, with provision for passing stored data from one to the next. Thus, in one embodiment, the CDMA code word correlator 340 of Fig 5 depicts a synchronous digital circuit such as would be implemented in a programmable logic device (PLD) or ASIC.

[0036] In Fig. 6, one embodiment of the transmitter 300 uses baseband demodulation to modify the shape of the correlation function of the received signal. Antenna 201 receives the ultra-wideband signal which is then bandpass filtered and amplified by amplifier 202. This signal is mixed in quadrature in mixers 203a and 203b resulting in real and imaginary parts of the complex incoming signal. The frequency of the local oscillator is chosen to approximate the frequency of the maximum spectral power density of the received signal from amplifier 202. The baseband signals from mixers 203a and 203b are filtered by low pass filters 610 and are delayed by time D in delays 21a and 21b, respectively. The outputs of delays 21a and 21b are then correlated with the undelayed signals from mixers 203a and 203b using analog multiplying correlators 22a, 22b, 22c, and 22d. The analog outputs from these correlators are subtracted and added in subtractor 220 and adder 221, respectively. The resulting analog signals from subtractor 220 and adder 221 can be seen to be an analog implementation of a complex correlation between the delayed and undelayed versions of the complex baseband signal from mixers 203a and 203b. The difference output of subtractor 220 is the real part, and the summed output of the adder 221 is the imaginary part of the complex correlated signal. Integrators 23a and 23b perform a complex integration which is digitized by ADCs 210a and 210b. The digitized results are sent to DSP 215. When implementing a receiver with multiple delay channels, then the items in the dotted line (21a-b, 22a-d, 23a-b, 210a-b, 220, 221) are repeated once for each different delay channel. Each receiver requires only one copy of antenna 201, amplifier 202, mixers 203a and 203b, local oscillator 204, phase shifter 205 and DSP 215.

[0037] The receiver 300 of Figure 6 calculates the phase angle and amplitude of the complex value formed by the values from ADCs 210a and 210b. The operation of estimating the phase angle of a sequence of complex values modulated by an information sequence can be performed either through the use of local bit decisions or by squaring the input data. The correction of the phase allows the complex output of ADCs 210a and 210b to be converted to a real number the sign of which depends on the phase angle calculated from ADCs 210a and 210b. The real data so produced is either positive or negative, depending upon the relative phases of the pulses in the

received pulse pairs, and so can be used in a manner which is completely analogous to the output of the receiver 100 depicted in Figure 4. The absolute value of this data is determined by the modulus of the correlation function at this mismatched delay, and so it is relatively insensitive to delay mismatch.

[0038] Note that if multiple delay channels are required are required in the receiver of Figure 6, the same I/Q converter can be shared by all the delay channels. Note also that if additional protection against delay variations is required, multiple delays per receiver channel can be implemented. For example, each delay channel could be replicated three times, once with the nominal delay, once with the nominal delay minus an offset and once with the nominal delay plus the same offset. For each transmitter being tracked, the best delays for each channel could be found by comparison of output energies.

[0039] Since the receiver 300 of Fig. 6 is operated by computing the autocorrelation of the input signal at a certain lag, the receiver 300 will also compute the autocorrelation at the same lag of any noise that is added to the signal. If the noise autocorrelation at that lag is non-zero, then it will produce an additive offset to the signal autocorrelation that will increase the bit error probability. This effect can be corrected in one of two ways, both of which require knowledge of the noise autocorrelation function. The first option is to specify the nominal delays at known zeros of the noise autocorrelation. The second is to subtract the known, non-zero noise correlation value from the output of the receiver prior to detection of bits. The noise autocorrelation function can be obtained from the frequency response functions of the front end filters that band limit the noise.

[0040] As an example, consider the power spectral densities plotted in Figure 7. This example will use a noise carrier. Figure 7 shows the power spectral density (PSD) of a noise carrier with a 2 gigahertz bandwidth and a center frequency of 2 gigahertz. This is the sample spectrum of a simulated carrier, formed by filtering uncorrelated noise sampled at 40 gigahertz with a 551-tap FIR filter, with the desired bandpass response. Figure 8 shows the same carrier modulated by a TR/DH CDMA code word 135. In one embodiment, the CDMA code word 135 is composed of

sixteen 600-nanosecond chips, each imposing correlation on the noise carrier at one of four lags: 1.65 nanoseconds, 2.65 nanoseconds, 3.65 nanoseconds and 4.65 nanoseconds. As shown in Fig. 8, the most noticeable effect of the TR/DH modulation is to raise the overall sidelobe level. It should be appreciated that the raised overall sidelobe levels shown in Fig. 8 can be filtered out using filter 175 (Fig. 1).

[0041] Figs. 9-12 depict the various stages in the demodulation of the noise signal that has a spectrum depicted in Figure 8. Figure 9 is a portion of the noisy signaling waveform, and the segment depicted has a duration of 25 nanoseconds. Figure 10 depicts the outputs of the four multipliers in the bank of correlators 320. Each correlator in the bank of correlators 320 has, for example, the structure depicted in Figure 4. Figure 10 depicts a time interval of 15 microseconds, during which the transmission of a single TR/DH code word of duration 9.6 microseconds takes place. The four pulse-pair correlators are tuned to the four delays used in the modulation: 1.65 nanoseconds, 2.65 nanoseconds, 3.65 nanoseconds and 4.65 nanoseconds. Note that the mean levels of the outputs of the multipliers shift away from zero at certain times; these times correspond to the times of the transmitted chips. Figure 11 depicts the outputs of the four integrators of the pulse-pair correlators. The waveforms are the actual chip waveforms arising from the simulation. The DH CDMA code 135 transmitted in this example can be expressed as an ordered sequence of integers {3, 4, 1, -4, -1, -2, 3, -2, 4, -1, -3, -2, -4, 1, 3, -4}. This sequence of numbers represents the numbers of the transmitted delays, numbered from shortest to longest, and the signs of the numbers denote the polarity of the transmitted chip. The CDMA code word 135 can be "read off" the waveforms depicted in Figure 11. For example, reading from left to right, the first channel to produce an output waveform is channel 3, and the polarity of that waveform is positive. Figure 12 shows the output of a DH CDMA code correlator 340 of the type depicted in Figure 3 when the input consists of the chip waveforms depicted in Figure 11. For this relatively short code, the code correlator output has high sidelobes. Other DH CDMA codes will have upwards of a thousand chips, and a much lower ratio of peak absolute sidelobe level to peak mainlobe level in the output correlation.

[0042] The foregoing discussion of the invention has been presented for purposes of illustration and description. Further, the description is not intended to limit the invention to the form disclosed herein. Consequently, variations and modifications commensurate with the above teachings and with the skill and knowledge of the relevant art are within the scope of the present invention. The embodiment described herein above is further intended to explain the best mode presently known of practicing the invention and to enable others skilled in the art to utilize the invention as such, or in other embodiments, and with the various modifications required by their particular application or uses of the invention. It is intended that the appended claims be construed to include alternative embodiments to the extent permitted by the prior art.

PARTS LIST

FIG. 1

- 100 transmitter
- 110 wideband noise source
- 130 information modulator
- 160 delay
- 170 summer
- 180 antenna

FIG. 2

- 135 delay hop CDMA code word chips
- 140 delay hop controller
- 145 information symbols
- 150 multiplexer switch
- 175 filter

FIG. 3

- 300 receiver
- 310 antenna
- 320 bank of correlators
- 330 analog to digital converter
- 340 CDMA code word correlator

350 receiver output

FIG. 4

321 delay

322 multiplier

326 integrator

FIG. 5

342 chip delay

344 adder

FIG. 6

21a delay

21b delay

22a multiplying correlator

22b multiplying correlator

22c multiplying correlator

22d multiplying correlator

23a integrator

23b integrator

101 I/Q converter

201 antenna

202 amplifier

RD-28,759

CONFIDENTIAL

203a mixer

203b mixer

204 oscillator

205 phase shifter

210a analog to digital converter

210b analog to digital converter

215 digital signal processor

220 subtractor

221 adder

610 low pass filter